

PARTICLE-LADEN FLOWS: SOME CONUNDRUMS

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SOME HISTORY

- Numerous papers (of variable quality) have been published
- Annual Review articles by Marple (1970) and Drew (1983)
- Einstein (1906) investigated these flows
- An early investigation involving the stability of plane Poiseuille flow made by Saffman (1962)
- Michael (1968) investigated the (inviscid) dusty flow past a sphere
- *Hydrodynamics of Suspensions* Ungarish (1993)
- *The Dynamics of Fluidized Particles* Jackson (2000)

(COMPREHENSIVE) EQUATIONS OF MOTION (A LA DREW, 1983)

Following Drew (1983)

$$\frac{\partial(\alpha_k \rho_k)}{\partial t} + \nabla \cdot (\alpha_k \rho_k \underline{v}_k) = 0$$

$$\begin{aligned} \frac{\partial(\alpha_k \rho_k \underline{v}_k)}{\partial t} + \nabla \cdot (\alpha_k \rho_k \underline{v}_k \underline{v}_k) &= -\alpha_k \nabla p_k + \nabla \cdot \left(\alpha_k (\underline{\tau}_k + \underline{\sigma}_k) \right) \\ &+ (\rho_{k,i} - \rho_k) \nabla \alpha_k + M_k \end{aligned}$$

$k = 1$: particles, $k = 2$: fluid. $\underline{\tau}_k$ is (approximately) stress tensor, $\underline{\sigma}_k$ turbulent stress tensor, $p_{k,i}$ pressure at interface, M_k 'interfacial' force density'; α , ρ , \underline{v} volume fraction, density and velocity fields.

SIMPLIFICATIONS

- Turbulent stresses $\underline{\underline{\sigma_k}} = 0$
- Drew (1983) states $p_{k,i} = p_k$ for non-acoustic problems
- Drew (1983) states $p_1 = p_2 + p_c$, where p_c pressure due to collisions; assume $p_1 = p_2$, and constant.
- Assume $\underline{\underline{\tau_1}} = 0$ for solid particles
- Must have $\alpha_1 + \alpha_2 = 1$, $M_1 + M_2 = 0$
- Will consider 3 problems

NON-DIMENSIONAL EQUATIONS OF MOTION

$\underline{u}_f, \underline{u}_p$ fluid, particle velocities

$$-\frac{\partial \alpha}{\partial t} + \nabla \cdot ((1 - \alpha)\underline{u}_f) = 0$$

$$\frac{\partial \underline{u}_f}{\partial t} + (\underline{u}_f \cdot \nabla)\underline{u}_f = -\nabla p + \frac{1}{Re} \frac{1}{1 - \alpha} \nabla \cdot ((1 - \alpha)\underline{e}) + \frac{\beta \alpha}{1 - \alpha} (\underline{u}_p - \underline{u}_f),$$

$$\frac{\partial \alpha}{\partial t} + \nabla \cdot (\alpha \underline{u}_p) = 0,$$

$$\frac{\partial \underline{u}_p}{\partial t} + (\underline{u}_p \cdot \nabla)\underline{u}_p = -\frac{1}{\gamma} \nabla p + \frac{\beta}{\gamma} (\underline{u}_f - \underline{u}_p)$$

Here $Re = UL/\nu$, $\beta = (9\nu L)/(2Ud^2)$ (Stokes drag), $\gamma = \rho_p/\rho_f$,
 \underline{e} rate of strain tensor for fluid.

PROBLEM 1: STEADY DUSTY INVISCID FLOW OVER A CIRCULAR CYLINDER

Cylinder version of sphere problem considered by Michael (1968) - fluid affects particles but not v.v.

Polar coordinates (r, θ) , velocity (u, v) , as $\alpha \rightarrow 0$:

$$(u_f(r, \theta), v_f(r, \theta))^T = \left(\left(1 - \frac{1}{r^2}\right) \cos \theta, -\left(1 + \frac{1}{r^2}\right) \sin \theta \right)^T$$

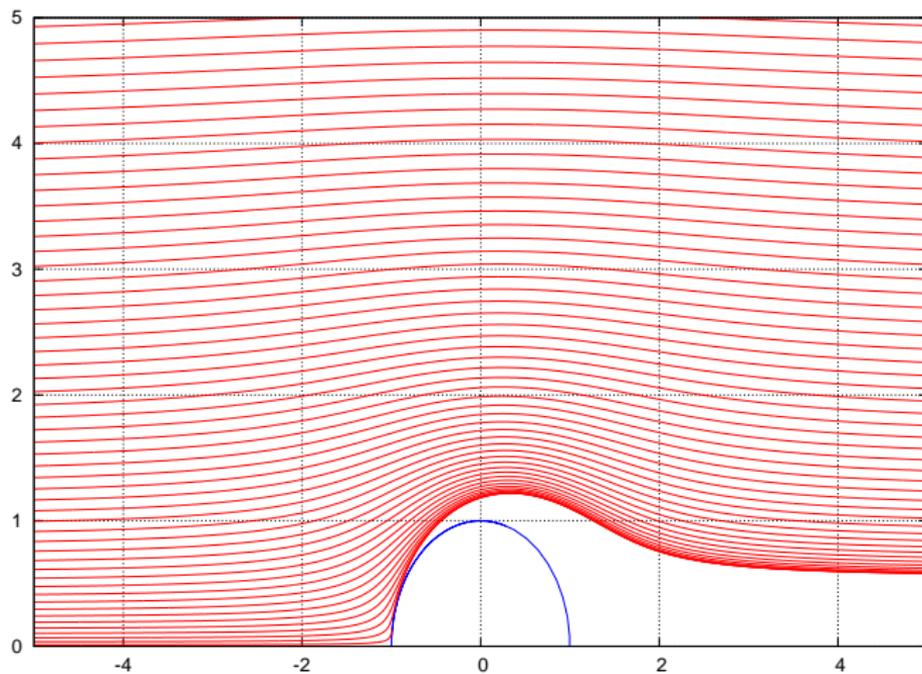
Then $\gamma \rightarrow \infty$ (heavy particles), $\gamma/\beta = O(1)$:

$$u_p \frac{\partial u_p}{\partial r} + \frac{v_p}{r} \frac{\partial u_p}{\partial \theta} - \frac{v_p^2}{r} = \frac{\beta}{\gamma} (u_f - u_p),$$

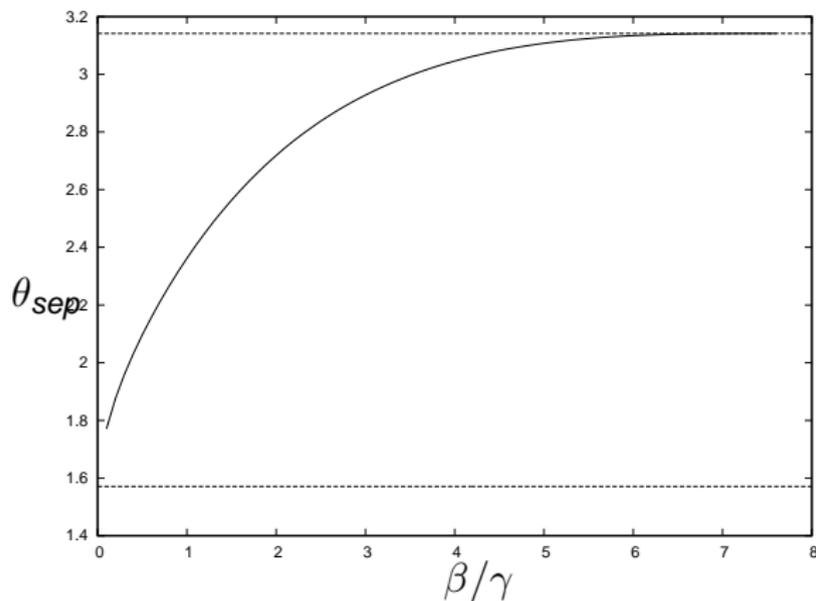
$$u_p \frac{\partial v_p}{\partial r} + \frac{v_p}{r} \frac{\partial v_p}{\partial \theta} + \frac{u_p v_p}{r} = \frac{\beta}{\gamma} (v_f - v_p),$$

$$\frac{1}{r} \frac{\partial}{\partial r} (r \alpha u_p) + \frac{1}{r} \frac{\partial}{\partial \theta} (\alpha v_p) = 0$$

PARTICLE PATHS, $\beta/\gamma = 5$

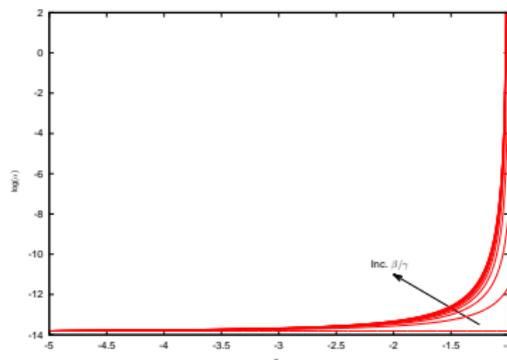
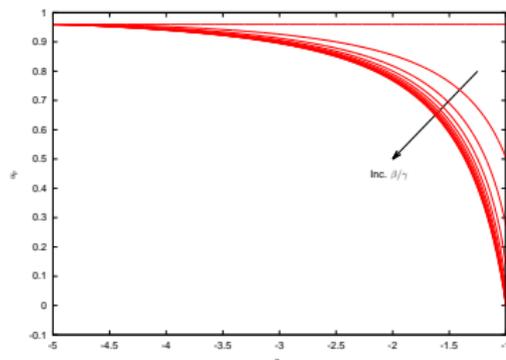


SEPARATION ANGLE



'Separation' angle θ_{sep} for increasing values of inter-phase drag parameter β/γ . Note as $\beta/\gamma \rightarrow 0^+$, $\theta_{sep} \rightarrow \pi/2$ and as $\beta/\gamma \rightarrow 8^-$, $\theta_{sep} \rightarrow \pi$, as shown as dashed lines

CONDITIONS ALONG $\theta = \pi$



As $r \rightarrow 1$, can show $u_p = u_{p0} + (r - 1)u_{p1} + \dots$, where

$$u_{p0} = 0, \quad u_{p1} = \frac{\beta}{2\gamma} \left(1 + \sqrt{1 - \frac{8\gamma}{\beta}} \right) \quad \text{for } \beta/\gamma < 8,$$

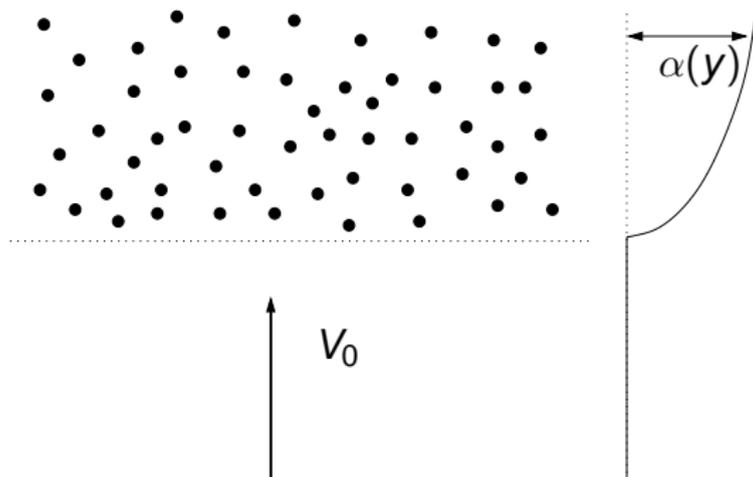
$$u_{p0} \neq 0, \quad u_{p1} = -\beta/\gamma \quad \text{for } \beta/\gamma > 8$$

ISSUES ARISING

- Particles can 'penetrate' cylinder surface
- Solution discontinuous at $\beta/\gamma = 8$
- 'Shadow' regions
- Since on $\theta = \pi$, $r\alpha u_p = \text{constant}$, if $u_p \rightarrow 0$, $\alpha \rightarrow \infty$:
violates $\alpha \ll 1$ condition
- A mixed elliptic/hyperbolic system

PROBLEM 2: SETTLING UNDER GRAVITY

Consider the stationary (1D) distribution of heavy ($\gamma \gg 1$) dust phase 'settling' under uniform gravity in an upwards propagating fluid; the dust-phase weight balanced by upwards motion of fluid. Fluid particle free and moving with constant speed V_0 for $y < 0$, $y = 0$ is location of stationary front.



INCLUDE (FLUID) VISCOSITY, AND (NOTIONALLY) ASSUME $\alpha = O(1)$

Problems of this type considered by Druzhinin (1994, 1995), with some inconsistencies.

Particles affect fluid and v.v. Problem reduces to

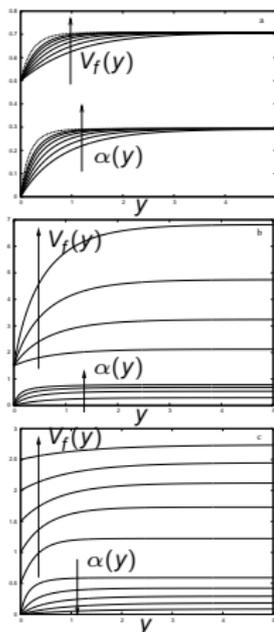
$$V_p = 0$$

$$((1 - \alpha)V_f)' = 0$$

$$V_f V_f' + \frac{V_f}{1 - \alpha} = \gamma - 1 + \frac{2}{Re} V_f'' - \frac{2}{Re} \frac{\alpha' V_f'}{1 - \alpha}$$

Assume $V_f(y = 0) = V_0$ (constant) and $\alpha(y = 0) = 0$.

(BASEFLOW) RESULTS FOR $V(y)$ AND $\alpha(y)$



(a): $\gamma = 2$, $V_0 = 0.5$, $Re = 1, 2, 4, 8, 16, 32$ (solid lines), the dashed lines show the $Re \gg 1$ solution, (b):

$V_0 = 1.5$, $Re = 20$, $\gamma = 4, 8, 16, 32$ and (c): $\gamma = 4$, $Re = 20$, $V_0 = 0.5, 1, 1.5, 2, 2.5$

SPATIAL LINEAR STABILITY IN THE INVISCID LIMIT

Can perturb the inviscid system for a steady base flow via

$$\alpha = \alpha_B(\mathbf{y}) + \epsilon \tilde{\alpha}(\mathbf{y}) e^{-i\omega t},$$

$$V_f = V_{fB}(\mathbf{y}) + \epsilon \tilde{v}_f(\mathbf{y}) e^{-i\omega t},$$

$$V_p = 0 + \epsilon \tilde{v}_p(\mathbf{y}) e^{-i\omega t},$$

Here $\epsilon \ll 1$, and ω is a real frequency.

Focus on $y \rightarrow \infty$:

$$\alpha_B \rightarrow \alpha_\infty = 1 - \sqrt{\frac{V_0}{\gamma - 1}}$$

$$V_f \rightarrow V_\infty = ((\gamma - 1)V_0)^{\frac{1}{2}}$$

LINEAR STABILITY IN THE INVISCID LIMIT (CONTINUED)

Further supposing $(\tilde{\alpha}(y), \tilde{v}_f(y), \tilde{v}_p(y)) = (\hat{\alpha}, \hat{v}_f, \hat{v}_p) e^{iky}$ Then

$$k^2 + k \left(-\frac{2\omega}{V_\infty} + \frac{2}{iV_\infty(1-\alpha_\infty)} \right) + \left(\frac{\omega^2(\gamma + \alpha_\infty(1-\gamma))}{\alpha_\infty V_\infty^2} - \frac{\omega}{iV_\infty^2 \alpha_\infty(1-\alpha_\infty)} \right) = 0$$

Considering the limit $\omega \rightarrow \infty$, we write $k = \omega K$, $K = O(1)$,

$$K = \frac{1}{V_\infty} \pm \frac{i}{V_\infty} \sqrt{\frac{\gamma(1-\alpha)}{\alpha_\infty}}$$

Spatial growth is

$$\exp \left(\frac{\omega \gamma^{\frac{1}{2}}}{(\gamma-1)^{\frac{3}{4}} V_0^{\frac{1}{4}}} \left(1 - \left(\frac{V_0}{(\gamma-1)} \right)^{\frac{1}{2}} \right)^{-\frac{1}{2}} y \right)$$

Spatial growth rate proportional to frequency - implies problem ill-posed.

LINEAR STABILITY, FINITE Re

Equation for k now a cubic:

$$k^3 \left(\frac{2\alpha_\infty V_\infty}{(1-\alpha_\infty)\omega Re} \right) + k^2 \left(\frac{iV_\infty^2 \alpha_\infty}{\omega(1-\alpha_\infty)} - \frac{2\alpha_\infty}{Re(1-\alpha_\infty)} \right) + k \left(\frac{2\alpha_\infty V_\infty}{(1-\alpha_\infty)^2 \omega} - \frac{2iV_\infty \alpha_\infty}{1-\alpha_\infty} \right) + \left(i\omega \left(\gamma + \frac{\alpha_\infty}{1-\alpha_\infty} \right) - \frac{1}{(1-\alpha_\infty)^2} \right) = 0$$

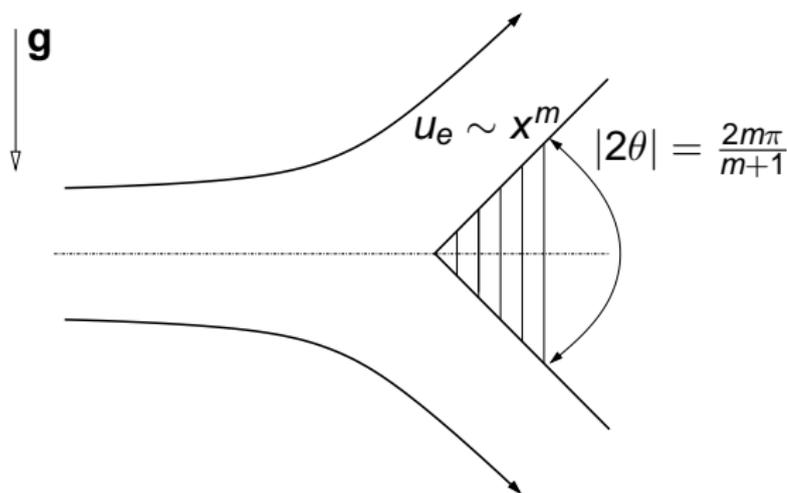
As $\omega \rightarrow \infty$, $Re = O(1)$, two families:-

$$k \rightarrow \pm \left(\frac{-(i\omega\gamma(1-\alpha_\infty) + \alpha_\infty)Re}{2\alpha_\infty} \right)^{\frac{1}{2}}$$

$$k \rightarrow \frac{\omega}{V_\infty} - \frac{i\gamma V_\infty(1-\alpha_\infty)Re}{2\alpha_\infty}$$

PROBLEM 3: BOUNDARY LAYERS IN A DILUTE PARTICLE SUSPENSION

Foster, Duck & Hewitt (2006) - mixed parabolic/hyperbolic problem



Flow geometry appropriate for Falkner–Skan-type edge conditions, although solutions not restricted to have self similarity. Assume that local gravitational forcing is aligned as shown and thus the upper boundary layer is such that

$\mathcal{K} > 0$ whilst the lower boundary layer has $\mathcal{K} < 0$, where $\mathcal{K} = \frac{gLRe^{1/2}}{U_\infty^2} \left(1 - \frac{1}{\gamma}\right)$

DUSTY BOUNDARY-LAYER EQUATIONS

Usual boundary-layer scalings

$$\begin{aligned}uu_x + vu_y + \bar{p}_x &= u_{yy} - \beta\alpha(u - u_p), \\u_p u_{px} + v_p u_{py} &= \frac{\beta}{\gamma}(u - u_p), \\u_p v_{px} + v_p v_{py} &= \frac{\beta}{\gamma}(v - v_p) - \mathcal{K} \cos \theta, \\u_x + v_y &= 0, \\u_p \alpha_x + v_p \alpha_y &= -\alpha(u_{px} + v_{py}).\end{aligned}$$

$$u = v = 0 \quad \text{on} \quad y = 0, \quad u \rightarrow u_e(x) \quad \text{as} \quad y \rightarrow \infty$$

Choice of boundary conditions for the particle phase is somewhat subtle; notionally

$$u_p \rightarrow u_{pe}(x), \quad \text{and} \quad \alpha \rightarrow \alpha_e(x), \quad \text{for} \quad y \rightarrow \infty.$$

Will consider $U_e(x) = x^m$, $0 \leq m \leq 1$

THE OUTER FLOW AND CONDITIONS AT THE BOUNDARY-LAYER EDGE

$$u_{pe}u'_{pe} = \frac{\beta}{\gamma}(u_e - u_{pe}), \quad u_{pe}E'_e + E_e^2 + \frac{\beta}{\gamma}E_e = -\frac{\beta}{\gamma}u'_e, \quad u_{pe}\alpha'_e + \alpha_e\mathcal{D}_e = 0, \quad (1)$$

where $E_e(x) = \partial v_p / \partial y (y \rightarrow \infty)$, $u_{pe}(x) = u_p(y \rightarrow \infty)$ and $\mathcal{D}_e(x) = \mathcal{D}(y \rightarrow \infty) = u'_{pe} + E_e$ are the relevant functions evaluated as $y \rightarrow \infty$. Also

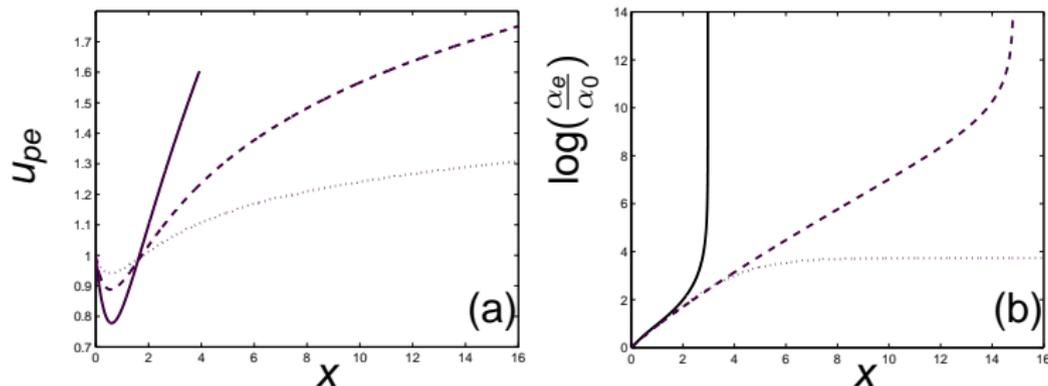
$$u_{pe}\mathcal{D}'_e + \frac{\beta}{\gamma}\mathcal{D}_e + (u'_{pe})^2 + E_e^2 = 0.$$

$$u_{pe} \left[u'_{pe} + \frac{\beta}{\gamma} \right] = \frac{\beta}{\gamma} u_e,$$

$$\left(u_{pe} \frac{d}{dx} + \frac{\beta}{\gamma} \right) \left(u_{pe} \frac{\alpha'_e}{\alpha_e} \right) = (u'_{pe})^2 + E_e^2.$$

For given fluid edge behaviour $u_e(x)$, can determine streamwise particle motion $u_{pe}(x)$, then particle motion normal to boundary E_e , and finally external volume fraction α_e

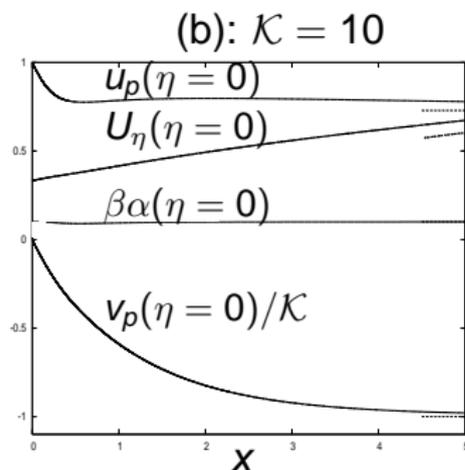
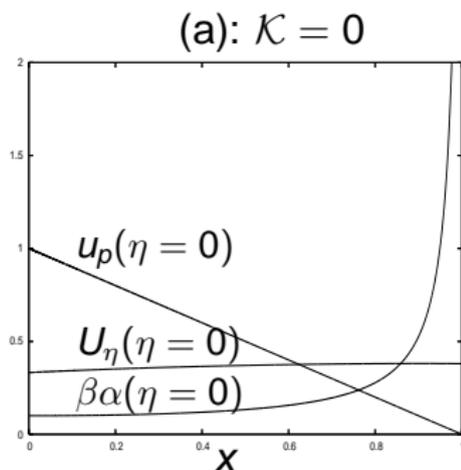
EDGE RESULTS



Development of the edge quantities (a) u_{pe} and (b) α_e ; solid $m = .50$; dashed $m = .211$; dotted $m = .10$, all with $\beta/\gamma = 1$; \mathcal{K} not relevant here.

Can show $\alpha_e \sim \frac{1}{x-x_0}$ if $m > m_{crit}$ - violates $\alpha \ll 1$

BOUNDARY-LAYER RESULTS



Development of wall values with x for $m = 0$, $\beta/\gamma = 1$. In case (b), leading-order asymptotic forms for $x \rightarrow \infty$ are shown for $x > 4.5$;

SINGULARITIES INSIDE THE BOUNDARY LAYER

Taking $\mathcal{K} = 0$ (for simplicity - particle flow can be solved explicitly on $y = 0$):

$$\alpha_w = \frac{\alpha_0}{U_{pw}} = \frac{\alpha_0}{1 - \frac{\beta x}{\gamma}}, \quad U_{pw} > 0.$$

Therefore volume fraction is singular part way along wall, and so model breaks down (Wang & Glass, 1988 continued their computation through the singularity).

Can be a 'race' between inner and outer singularities.

$$\mathcal{K} < 0$$

If gravitational forces act away from the wall, close to wall characteristics directed outwards; local analysis (as $x \rightarrow 0$) reveals a discontinuity in α along $y = y_{crit} = -\mathcal{K} \cos \theta / U_{p0}$ where $u_p = U_{p0} + \dots$:
for $y < y_{crit}$, $\alpha = 0$ (particle free), for $y > y_{crit}$, $\alpha = \alpha_0$

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- Computations and analyses inform each other
- Contaminants can have a profound effect!